

1 **Supplementary material for “Optically stimulated luminescence dating of heat retainer**  
2 **hearthths from the Sahara: Insights into signal accumulation and measurement.” Armitage et**  
3 **al.**

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5 **A. Sample preparation procedure**

6 Having removed the light exposed layers of the heat retainer, dating samples were prepared using  
7 standard laboratory techniques. Briefly, carbonate was removed by immersion in 1.16 M HCl,  
8 followed by immersion in H<sub>2</sub>O<sub>2</sub> to oxidise organic material. Samples FZ84, 85, 95 and 96 were sieved  
9 at 40 µm, and the material which passed through the mesh was subsequently Stokes settled to 4-11,  
10 11-20 and 20-40 µm. Material retained in the mesh was sieved to yield 40-60, 60-90, 90-125, 125-  
11 150, 150-180 and 180-210 size fractions. Quartz was extracted from the <90 µm fractions via  
12 prolonged immersion in H<sub>2</sub>SiF<sub>6</sub>. Quartz was extracted from the >90 µm fractions via density  
13 separation at 2.62 and 2.75 g/cm<sup>3</sup>, and 1 hour immersion in 23 M HF. Following H<sub>2</sub>SiF<sub>6</sub> or HF  
14 treatment, samples were immersed 11 M HCl for a minimum of 12 hours to remove fluoride  
15 precipitates. The <60 µm fractions were settled from suspension onto 10 mm diameter aluminium  
16 discs, resulting in a monolayer of quartz across the entire upper face of the disc. The >60 µm fractions  
17 were mounted on aluminium discs using Silkospray silicone oil applied via a 5 mm mask, resulting  
18 in a monolayer of grains across the middle 5 mm of the disc. Single-grain analysis was performed on  
19 180-210 µm grains mounted in Risø single-grain sample holders, containing a 10x10 array of 300 µm  
20 diameter holes. Sample preparation and mounting methods are summarised in Table S1.

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22 Table S1. Summary sample preparation and mounting methods for the various grain size fractions reported in this study.

Grain size (µm)	Size separation method	Quartz purification method	Sample mounting method
4-11			
11-20	Stokes settling		Settled from suspension
20-40		H <sub>2</sub> SiF <sub>6</sub> + HCl	
40-60			
60-90			
90-125	Sieve		Silkospray silicone oil via a 5 mm mask
125-150		Density separation + HF	
150-180			
180-210			

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24 **B. Single-grain rejection criteria.**

25 Grains were rejected where one or more of the following conditions are met: (1) the T<sub>n</sub> signal from  
26 the grain is too low to distinguish it from the variability in the background signal (the difference  
27 between T<sub>n</sub> and the average count from the background interval is less than three times the standard  
28 deviation of the counts in the background interval, determined using the “sig. >3 sigma above BG”  
29 rejection criterion in Luminescence Analyst, (Duller, 2007)); (2) the recycling ratio (Murray and  
30 Wintle, 2000) differs from unity by greater than 10%; (3) the OSL IR-depletion ratio (Duller, 2003)  
31 is greater than two standard errors below unity; (4) recuperation is high (i.e. L<sub>x</sub>/T<sub>x</sub> for the 0 Gy  
32 regeneration point is greater than 5% of L<sub>n</sub>/T<sub>n</sub>, (Murray and Wintle, 2000)); (5) L<sub>n</sub>/T<sub>n</sub> does not  
33 intercept the growth curve (Armitage et al., 2000; Bailey et al., 2005) – no grains failed this criterion  
34 due to the low D<sub>e</sub> of the samples, or (6) the dose response curve shape precludes the generation of a  
35 meaningful equivalent dose. Unlike the other five criteria, criterion six requires user-judgement and  
36 hence cannot be applied mechanistically. It was used where the signal does not increase  
37 monotonically in response to increasing dose, or where L<sub>n</sub>/T<sub>n</sub> intercepted the dose-response curve at  
38 the point where growth ceased, with the former being more common.

41 **C. Equivalent dose, dose rate and calculated age for different size fractions from Al Wafa heat**  
 42 **retainers.**

43 Equivalent dose ( $D_e$ ), dose rate and calculated age data for different size fractions from Al Wafa heat  
 44 retainers are presented in Tables S2-S5. In these tables, “Mean 4-210” denotes the mean age  
 45 determined for grain size fraction in the range 4-210  $\mu\text{m}$ . The “effective grain size” is calculated as  
 46 the grain size with a dose rate which yields the mean 4-210  $\mu\text{m}$  age for the 4-11  $\mu\text{m}$  quartz produced  
 47 by crushing the bulk sample (Section 5). Dose rates and ages are calculated using a mean water  
 48 content of  $5\pm 2\%$ , a burial depth of 30 cm (yielding a cosmic dose rate of  $0.235\pm 0.020$  Gy/ka) and  
 49 partitioning the gamma dose between the heat retainer and underlying sediments (Armitage and King,  
 50 2013). For alpha dose rates, an a-value of  $0.04 \pm 0.02$  was used throughout. Instrumental beta dose  
 51 rates were corrected for grain size using the values measured by Armitage and Bailey (2005, Table  
 52 1).

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Table S2: Heat retainer FZ84

Grain size ( $\mu\text{m}$ )	$D_e$ (Gy)	Dose rates (Gy/ka)				Age (ka)
		Alpha	Beta	Gamma	Total	
4-11	$7.5 \pm 0.2$	$0.10 \pm 0.05$	$0.41 \pm 0.04$	$0.23 \pm 0.02$	$0.98 \pm 0.07$	$7.7 \pm 0.6$
11-20	$7.9 \pm 0.2$	$0.08 \pm 0.04$	$0.41 \pm 0.04$	$0.23 \pm 0.02$	$0.96 \pm 0.07$	$8.3 \pm 0.6$
20-40	$7.1 \pm 0.2$	$0.06 \pm 0.03$	$0.40 \pm 0.04$	$0.23 \pm 0.02$	$0.93 \pm 0.06$	$7.7 \pm 0.5$
40-60	$7.4 \pm 0.2$	$0.04 \pm 0.02$	$0.40 \pm 0.04$	$0.23 \pm 0.02$	$0.90 \pm 0.05$	$8.2 \pm 0.6$
60-90	$6.9 \pm 0.2$	$0.03 \pm 0.01$	$0.39 \pm 0.04$	$0.23 \pm 0.02$	$0.88 \pm 0.05$	$7.8 \pm 0.5$
90-125	$6.5 \pm 0.2$	-	$0.39 \pm 0.04$	$0.23 \pm 0.02$	$0.85 \pm 0.05$	$7.7 \pm 0.5$
125-150	$6.4 \pm 0.2$	-	$0.38 \pm 0.04$	$0.23 \pm 0.02$	$0.84 \pm 0.05$	$7.6 \pm 0.5$
150-180	$6.1 \pm 0.2$	-	$0.37 \pm 0.04$	$0.23 \pm 0.02$	$0.84 \pm 0.05$	$7.3 \pm 0.5$
180-210	$6.4 \pm 0.2$	-	$0.37 \pm 0.04$	$0.23 \pm 0.02$	$0.83 \pm 0.05$	$7.7 \pm 0.5$
<b>Mean 4-210</b>	-	-	-	-	-	<b><math>7.8 \pm 0.5</math></b>
Effective grain size 40-60 $\mu\text{m}$						
<b>4-11 (crushed)</b>	<b><math>7.0 \pm 0.2</math></b>				<b><math>0.90 \pm 0.05</math></b>	<b><math>7.8 \pm 0.5</math></b>

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Table S3: Heat retainer FZ85

Grain size ( $\mu\text{m}$ )	$D_e$ (Gy)	Dose rates (Gy/ka)				Age (ka)
		Alpha	Beta	Gamma	Total	
4-11	$10.7 \pm 0.3$	$0.10 \pm 0.05$	$0.37 \pm 0.04$	$0.22 \pm 0.02$	$0.93 \pm 0.07$	$11.5 \pm 0.9$
11-20	$10.8 \pm 0.3$	$0.09 \pm 0.04$	$0.36 \pm 0.04$	$0.22 \pm 0.02$	$0.91 \pm 0.07$	$11.9 \pm 0.9$
20-40	$10.1 \pm 0.3$	$0.06 \pm 0.03$	$0.36 \pm 0.04$	$0.22 \pm 0.02$	$0.88 \pm 0.06$	$11.5 \pm 0.8$
40-60	$9.6 \pm 0.3$	$0.04 \pm 0.02$	$0.35 \pm 0.04$	$0.22 \pm 0.02$	$0.85 \pm 0.05$	$11.3 \pm 0.8$
60-90	$9.4 \pm 0.3$	$0.03 \pm 0.01$	$0.35 \pm 0.04$	$0.22 \pm 0.02$	$0.84 \pm 0.05$	$11.3 \pm 0.7$
90-125	$8.6 \pm 0.3$	-	$0.34 \pm 0.04$	$0.22 \pm 0.02$	$0.80 \pm 0.05$	$10.7 \pm 0.7$
125-150	$8.6 \pm 0.3$	-	$0.34 \pm 0.04$	$0.22 \pm 0.02$	$0.80 \pm 0.05$	$10.8 \pm 0.7$
150-180	$8.3 \pm 0.3$	-	$0.33 \pm 0.04$	$0.22 \pm 0.02$	$0.79 \pm 0.05$	$10.5 \pm 0.7$
180-210	$8.9 \pm 0.3$	-	$0.33 \pm 0.04$	$0.22 \pm 0.02$	$0.79 \pm 0.04$	$11.3 \pm 0.7$
<b>Mean 4-210</b>	-	-	-	-	-	<b><math>11.2 \pm 0.8</math></b>
Effective grain size 40-60 $\mu\text{m}$						
<b>4-11 (crushed)</b>	<b><math>9.5 \pm 0.3</math></b>				<b><math>0.85 \pm 0.05</math></b>	<b><math>11.2 \pm 0.8</math></b>

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Table S4: Heat retainer FZ95

Grain size ( $\mu\text{m}$ )	$D_e$ (Gy)	Dose rates (Gy/ka)				Age (ka)
		Alpha	Beta	Gamma	Total	
4-11	$5.8 \pm 0.2$	$0.07 \pm 0.04$	$0.32 \pm 0.03$	$0.22 \pm 0.02$	$0.85 \pm 0.06$	$6.9 \pm 0.5$
11-20	$9.4 \pm 0.3$	$0.06 \pm 0.03$	$0.32 \pm 0.03$	$0.22 \pm 0.02$	$0.83 \pm 0.05$	$11.3 \pm 0.8^*$
20-40	$4.1 \pm 0.1$	$0.04 \pm 0.02$	$0.31 \pm 0.03$	$0.22 \pm 0.02$	$0.81 \pm 0.05$	$5.1 \pm 0.3$
40-60	$4.8 \pm 0.1$	$0.03 \pm 0.01$	$0.31 \pm 0.03$	$0.22 \pm 0.02$	$0.79 \pm 0.04$	$6.1 \pm 0.4$
60-90	$4.8 \pm 0.1$	$0.02 \pm 0.01$	$0.31 \pm 0.03$	$0.22 \pm 0.02$	$0.77 \pm 0.04$	$6.2 \pm 0.4$
90-125	$4.3 \pm 0.1$	-	$0.30 \pm 0.03$	$0.22 \pm 0.02$	$0.75 \pm 0.04$	$5.7 \pm 0.4$
125-150	$4.6 \pm 0.1$	-	$0.29 \pm 0.03$	$0.22 \pm 0.02$	$0.75 \pm 0.04$	$6.2 \pm 0.4$
150-180	$6.2 \pm 0.2$	-	$0.29 \pm 0.03$	$0.22 \pm 0.02$	$0.74 \pm 0.04$	$8.4 \pm 0.5$
180-210	$4.4 \pm 0.1$	-	$0.29 \pm 0.03$	$0.22 \pm 0.02$	$0.74 \pm 0.04$	$6.0 \pm 0.4$
<b>Mean 4-210</b>	-	-	-	-	-	<b><math>6.3 \pm 1.0</math></b>
Effective grain size 90-150 $\mu\text{m}$						
<b>4-11 (crushed)</b>	<b><math>4.7 \pm 0.1</math></b>				<b><math>0.75 \pm 0.04</math></b>	<b><math>6.3 \pm 0.4</math></b>

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\*The age for 11-20  $\mu\text{m}$  grain size has been omitted from the calculation of the mean age.

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Table S5: Heat retainer FZ96

Grain size ( $\mu\text{m}$ )	$D_e$ (Gy)	Dose rates (Gy/ka)				Age (ka)
		Alpha	Beta	Gamma	Total	
4-11	$7.9 \pm 0.2$	$0.07 \pm 0.04$	$0.53 \pm 0.06$	$0.24 \pm 0.02$	$1.09 \pm 0.07$	$7.3 \pm 0.5$
11-20	$8.4 \pm 0.2$	$0.06 \pm 0.03$	$0.53 \pm 0.06$	$0.24 \pm 0.02$	$1.07 \pm 0.07$	$7.9 \pm 0.6$
20-40	$7.4 \pm 0.2$	$0.04 \pm 0.02$	$0.52 \pm 0.06$	$0.24 \pm 0.02$	$1.04 \pm 0.07$	$7.1 \pm 0.5$
40-60	$6.9 \pm 0.2$	$0.03 \pm 0.02$	$0.51 \pm 0.06$	$0.24 \pm 0.02$	$1.02 \pm 0.06$	$6.8 \pm 0.5$
60-90	$6.3 \pm 0.2$	$0.02 \pm 0.01$	$0.51 \pm 0.05$	$0.24 \pm 0.02$	$1.00 \pm 0.06$	$6.3 \pm 0.4$
90-125	$6.7 \pm 0.2$	-	$0.50 \pm 0.05$	$0.24 \pm 0.02$	$0.98 \pm 0.06$	$6.9 \pm 0.5$
125-150	$6.2 \pm 0.2$	-	$0.49 \pm 0.05$	$0.24 \pm 0.02$	$0.97 \pm 0.06$	$6.4 \pm 0.4$
150-180	$5.9 \pm 0.2$	-	$0.48 \pm 0.05$	$0.24 \pm 0.02$	$0.96 \pm 0.06$	$6.1 \pm 0.4$
180-210	$5.9 \pm 0.2$	-	$0.47 \pm 0.05$	$0.24 \pm 0.02$	$0.95 \pm 0.06$	$6.2 \pm 0.4$
<b>Mean 4-210</b>	-	-	-	-	-	<b><math>6.8 \pm 0.6</math></b>
Effective grain size $>210 \mu\text{m}$						
<b>4-11 (crushed)</b>	<b><math>5.9 \pm 0.2</math></b>				<b><math>0.87 \pm 0.06</math></b>	<b><math>6.8 \pm 0.5</math></b>

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**D. Single grain overdispersion values**

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Table S6: Single-grain equivalent dose, dose recovery and overdispersion data.

Sample	Equivalent dose data			Dose recovery data			
	$D_e$ (Gy)	Grains (accepted/measured)	$OD_{D_e}$ (%)	Ratio (recovered/known)	Grains (accepted/measured)	$OD_{Rec}$ (%)	$OD_{\beta}$ (%)
FZ40	$9.2 \pm 0.3$	131/1000	$18.5 \pm 1.5$	$0.98 \pm 0.02$	135/1200	$9.7 \pm 1.1$	$15.8 \pm 1.8$
FZ47	$7.3 \pm 0.3$	89/1200	$24.9 \pm 2.3$	$0.99 \pm 0.01$	164/1200	$7.7 \pm 0.7$	$23.7 \pm 2.4$
FZ84	$6.0 \pm 0.1$	171/1200	$26.5 \pm 1.6$	$1.00 \pm 0.01$	242/1200	$7.5 \pm 0.7$	$25.4 \pm 1.8$
FZ85	$8.6 \pm 0.1$	262/1200	$21.0 \pm 1.1$	$0.96 \pm 0.01$	276/1200	$6.3 \pm 0.6$	$20.0 \pm 1.2$
FZ95	$4.5 \pm 0.1$	242/1100	$28.2 \pm 1.5$	$0.98 \pm 0.01$	281/1200	$7.9 \pm 0.7$	$27.1 \pm 1.6$
FZ96	$6.0 \pm 0.1$	176/1200	$24.5 \pm 1.5$	$0.99 \pm 0.01$	195/1200	$6.3 \pm 0.8$	$23.7 \pm 1.7$

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72 **E. Equivalent doses for uncrushed and crushed quartz separates**

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Table S7: Sample description and equivalent doses for uncrushed and crushed fractions of zero-age quartzes.

Sample	Provenance	Equivalent dose (Gy)		Increase (Gy) (crushed-uncrushed)
		Uncrushed	Crushed	
BA5	Coastal dune (Armitage et al., 2006)	0.04 ± 0.01	0.23 ± 0.02	0.19 ± 0.02
CH62	Shoreline (Armitage et al., 2015)	0.01 ± 0.01	0.11 ± 0.02	0.10 ± 0.02
FZ16	Desert dune (Armitage et al., 2007)	0.04 ± 0.03	0.12 ± 0.04	0.08 ± 0.05
FZ32	Desert dune (Armitage and Bailey, 2005)	0.08 ± 0.08	0.16 ± 0.08	0.08 ± 0.12
IN22	Coastal dune (Armitage et al., 2006)	0.01 ± 0.02	0.02 ± 0.01	0.01 ± 0.02
Risø quartz	Calibration sample (Hansen et al., 2015)	0.00 ± 0.00	0.09 ± 0.01	0.09 ± 0.01
SA10	Coastal dune (this study)	0.00 ± 0.00	0.93 ± 0.33	0.93 ± 0.33
			<b>Mean</b>	<b>0.21 ± 0.12</b>

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Table S8: Sample description and equivalent doses for uncrushed and crushed fractions of Holocene quartzes.

Sample	Provenance	Equivalent dose (Gy)		Ratio (uncrushed/crushed)
		Uncrushed	Crushed	
CH22	Shoreline (Armitage et al., 2015)	3.72 ± 0.13	4.07 ± 0.19	1.09 ± 0.06
IN15	Coastal dune (Armitage et al., 2006)	5.35 ± 0.07	5.31 ± 0.06	0.99 ± 0.02
IN16	Coastal dune (Armitage et al., 2006)	2.34 ± 0.11	2.53 ± 0.12	1.08 ± 0.07
NG38	Shoreline (Armitage et al., 2015)	19.5 ± 0.2	20.3 ± 1.2	1.04 ± 0.06
NG39	Shoreline (Armitage et al., 2015)	19.1 ± 0.8	19.4 ± 0.5	1.02 ± 0.05
			<b>Mean</b>	<b>1.04 ± 0.02</b>

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